
Exploring the Physics of the Electric Arc Furnaces

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RHI MAGNESITA





Outline

- Introduction of EAF Model
- Single phase electric arc
- Arc impingement 3-phase flow
- Closing remarks

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Introduction of EAF Model

- The model presented aims to model the processes occurring inside electric arc furnace
- This model is capable of solving the flow, turbulence, thermal and electromagnetic field in **coupled** fashion.
- As the first step the model aims to optimize **DC-EAF** through 2D axisymmetric simulations
- The electromagnetic field is solved in the domain using the induction method
- The model accounts for **multiphase-flow** simulation and the interaction between air (plasma), slag and liquid metal

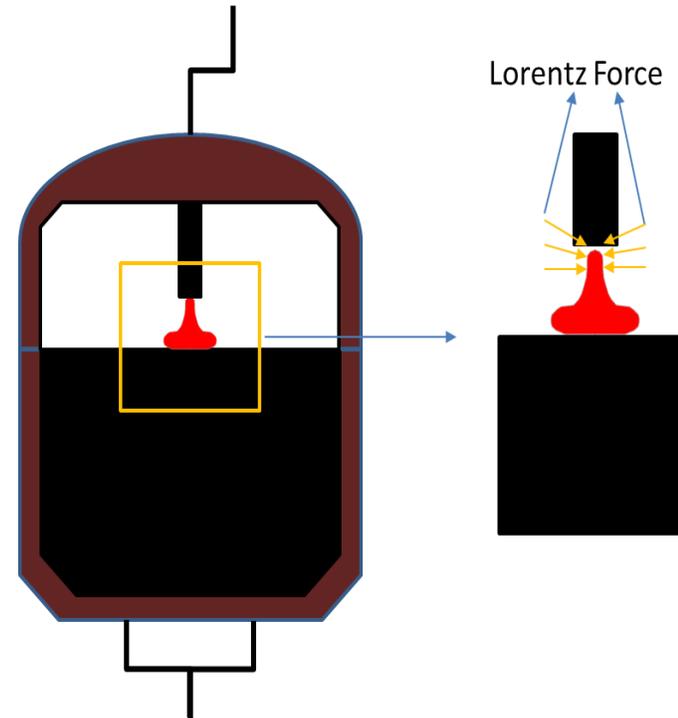
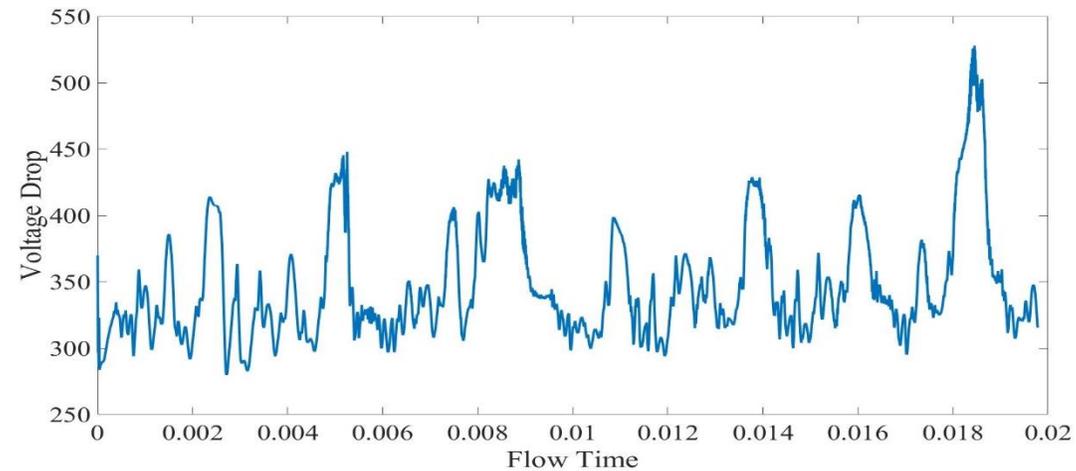
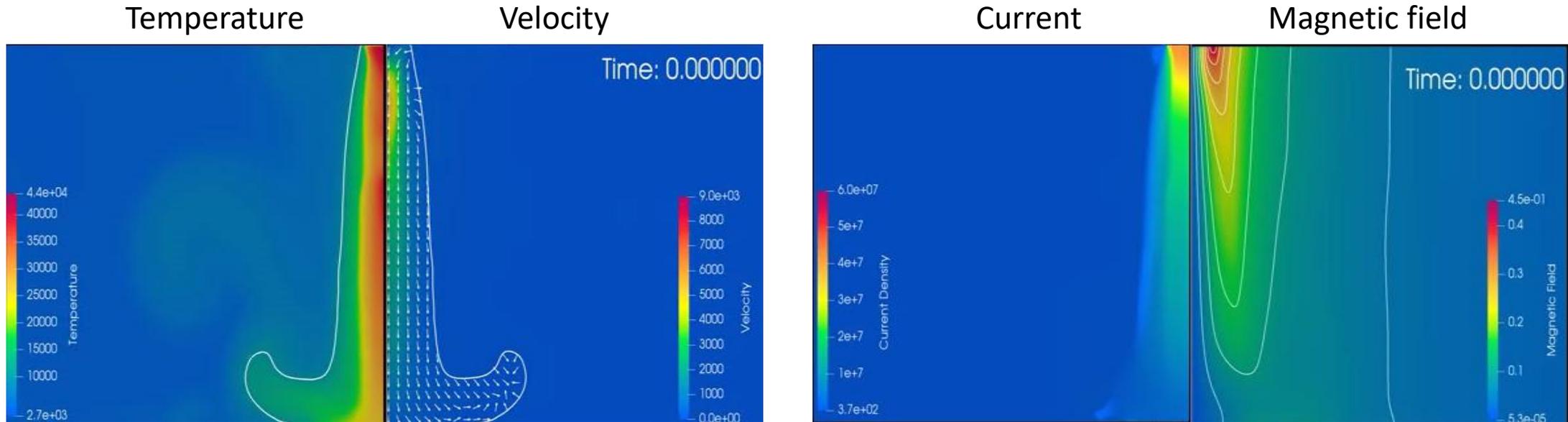


Figure 1: Simplified DC EAF schematic

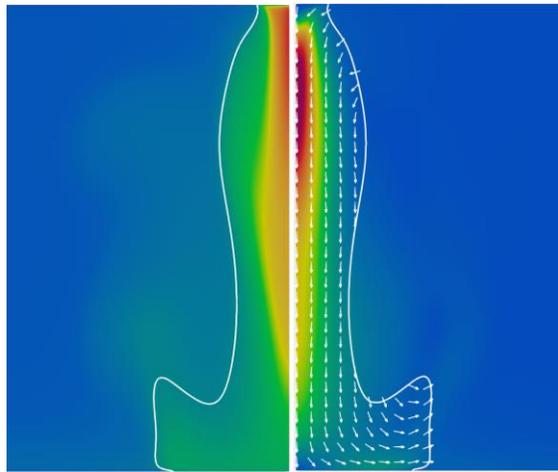
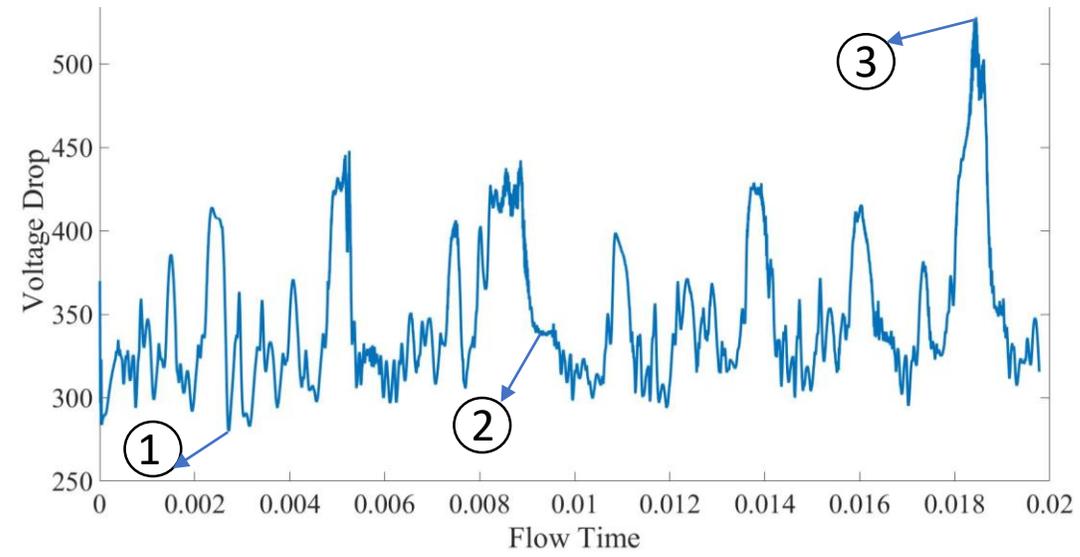
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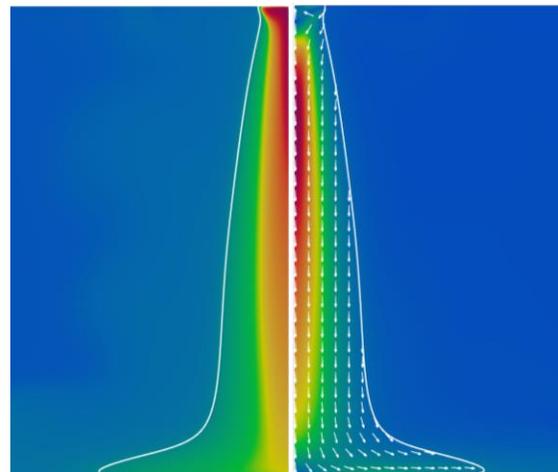
Incompressible model (single phase simulation)



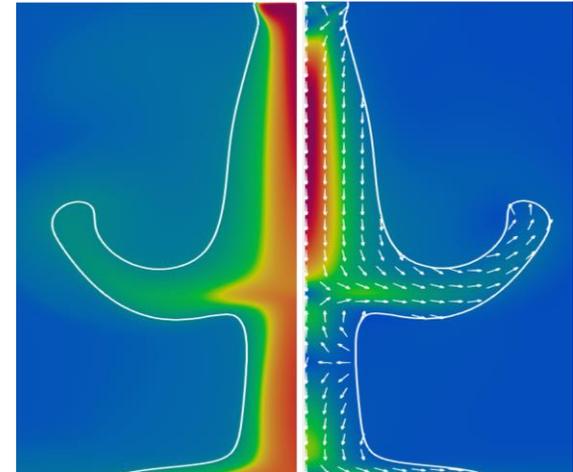
$$\Delta\phi = \frac{1}{I_0} \sum \frac{J_z^2 + J_r^2}{\sigma} \Delta V$$



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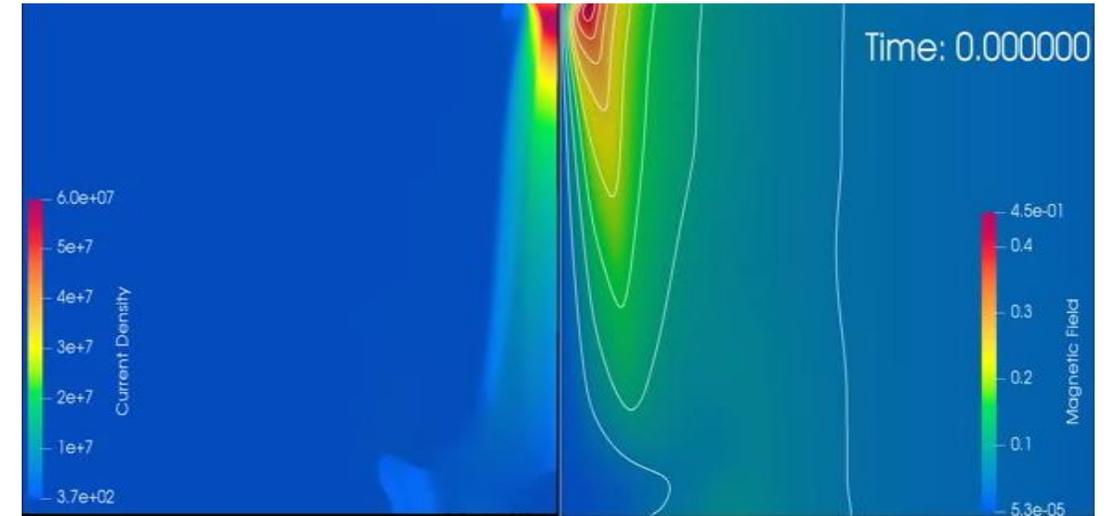
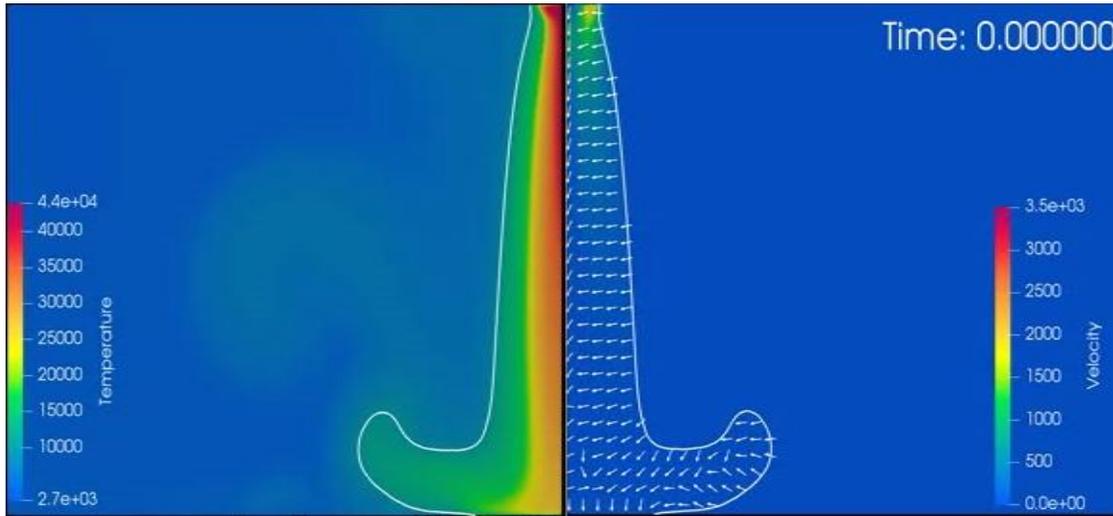
Compressible: Ideal Gas Model (single phase simulation)

Temperature

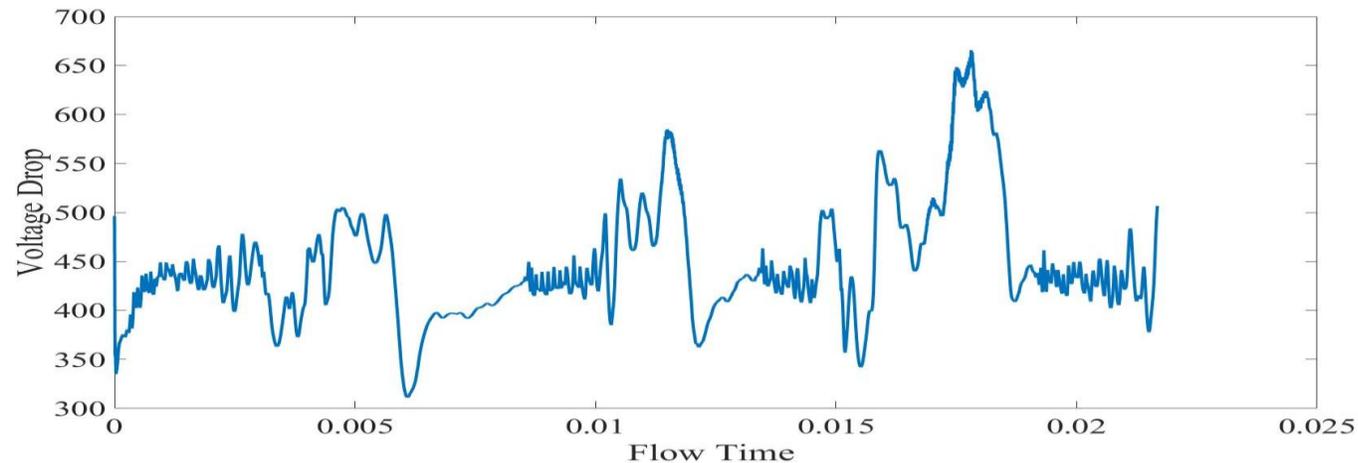
Velocity

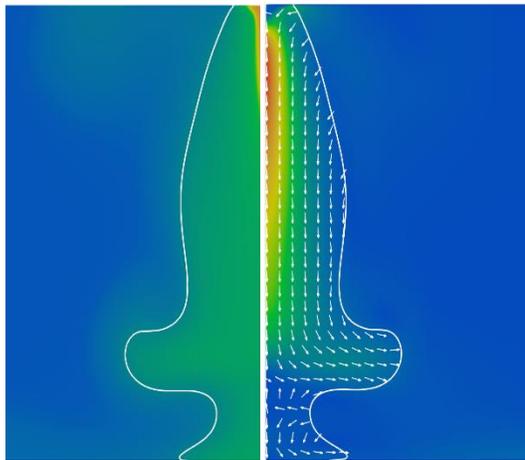
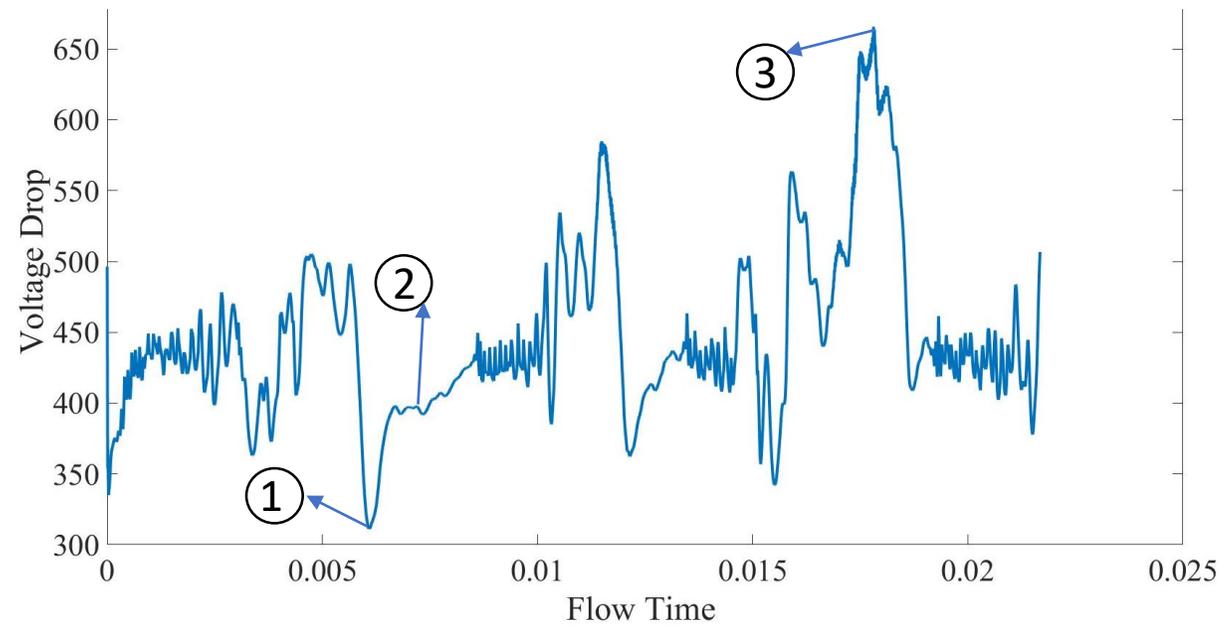
Current

Magnetic field

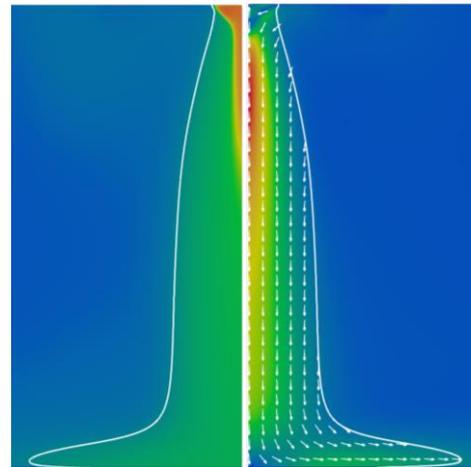


$$\Delta\phi = \frac{1}{I_0} \sum \frac{J_z^2 + J_r^2}{\sigma} \Delta V$$

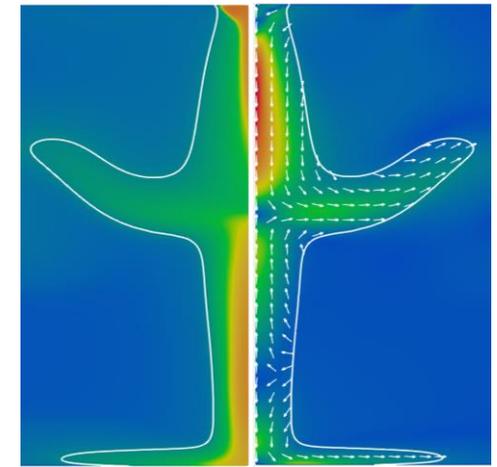




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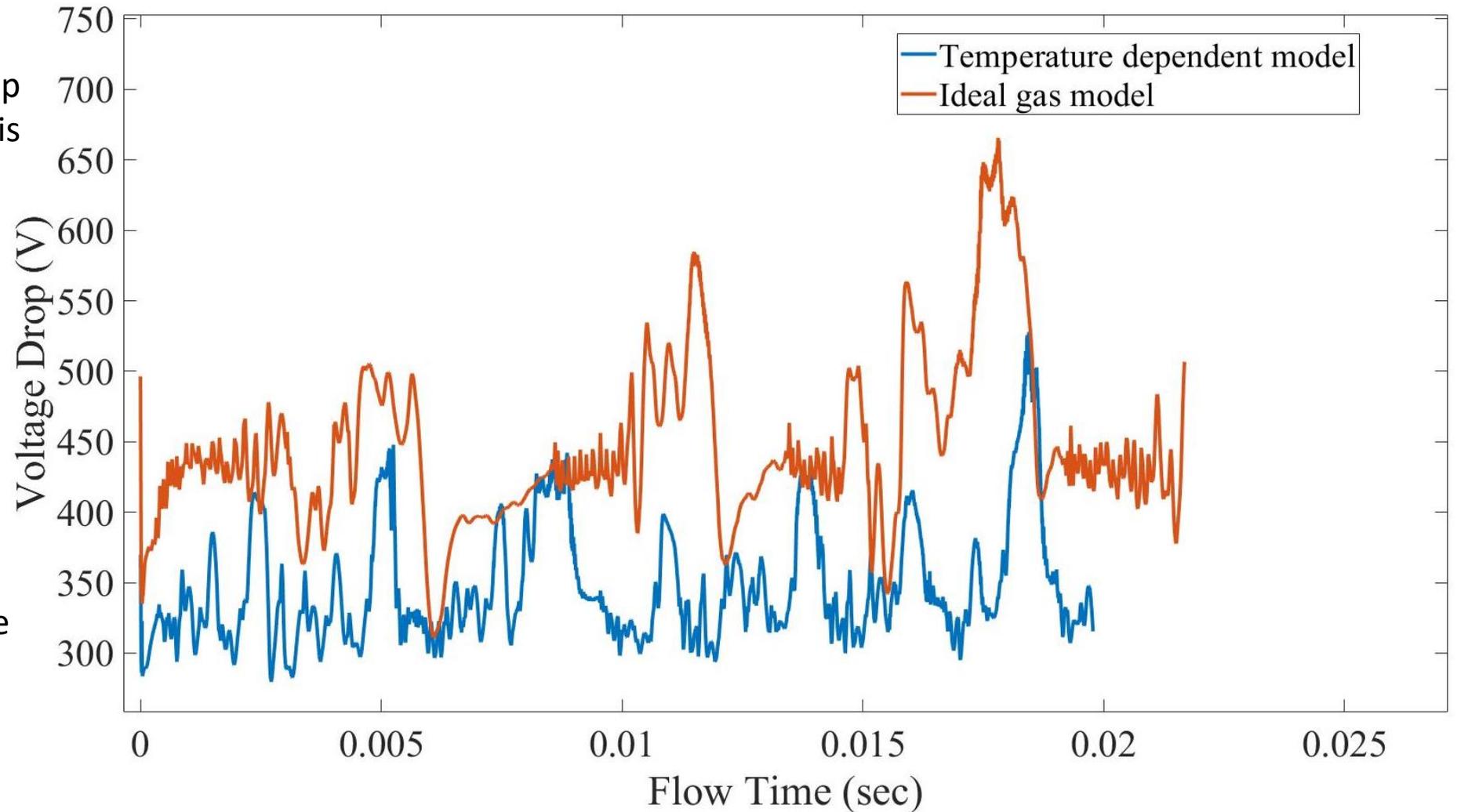
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Comparison between Voltage Drop between compressible and incompressible flow

- The average voltage drop of incompressible flow is 320 V
- Compressible flow have a voltage drop of 430 V
- Difference is 110 V significant
- The compressible flow seems to have repetitive voltage drop pattern



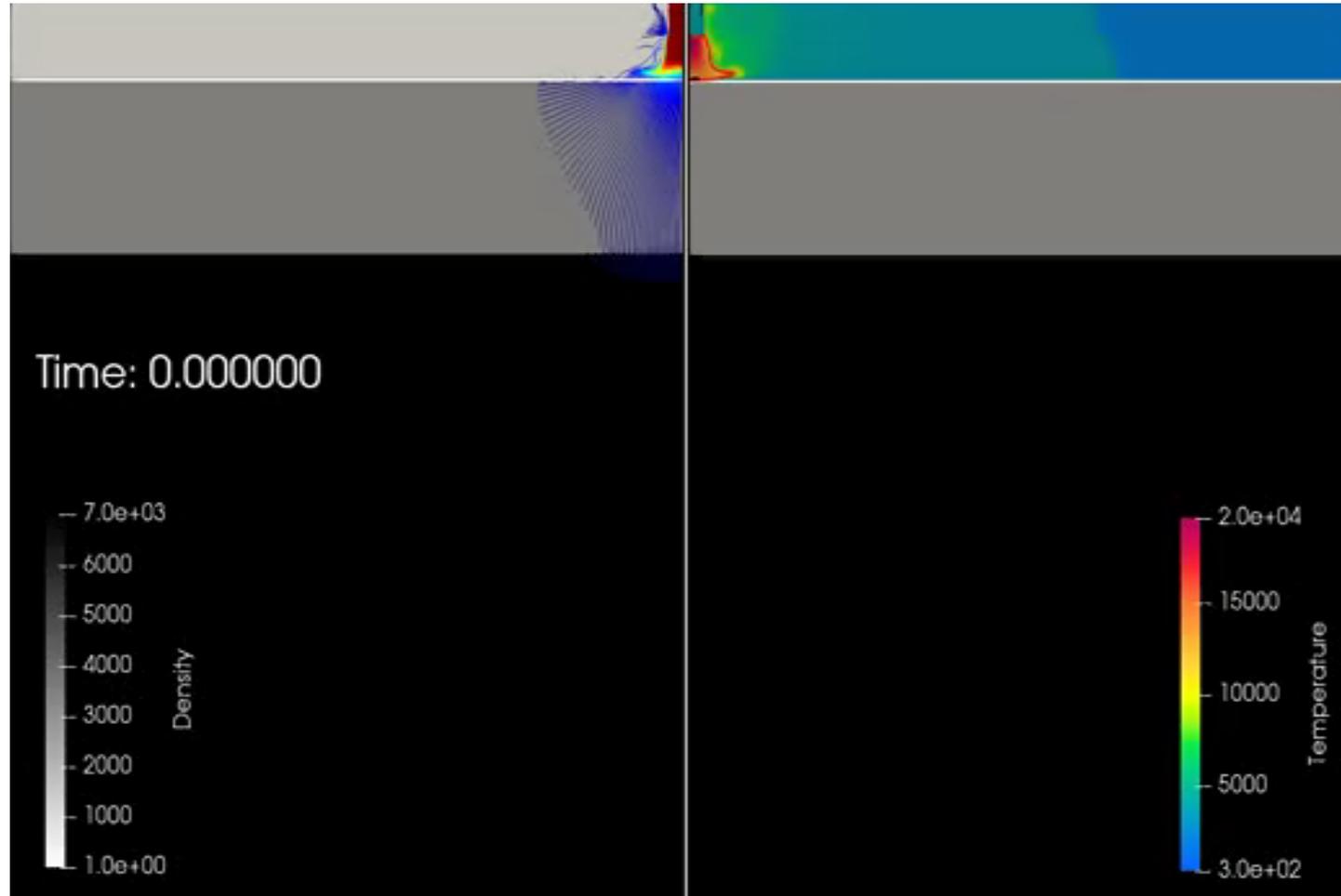
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10 kAmp Arc Impingement

I = 10 K amps

Arc Gap = 0.05 m



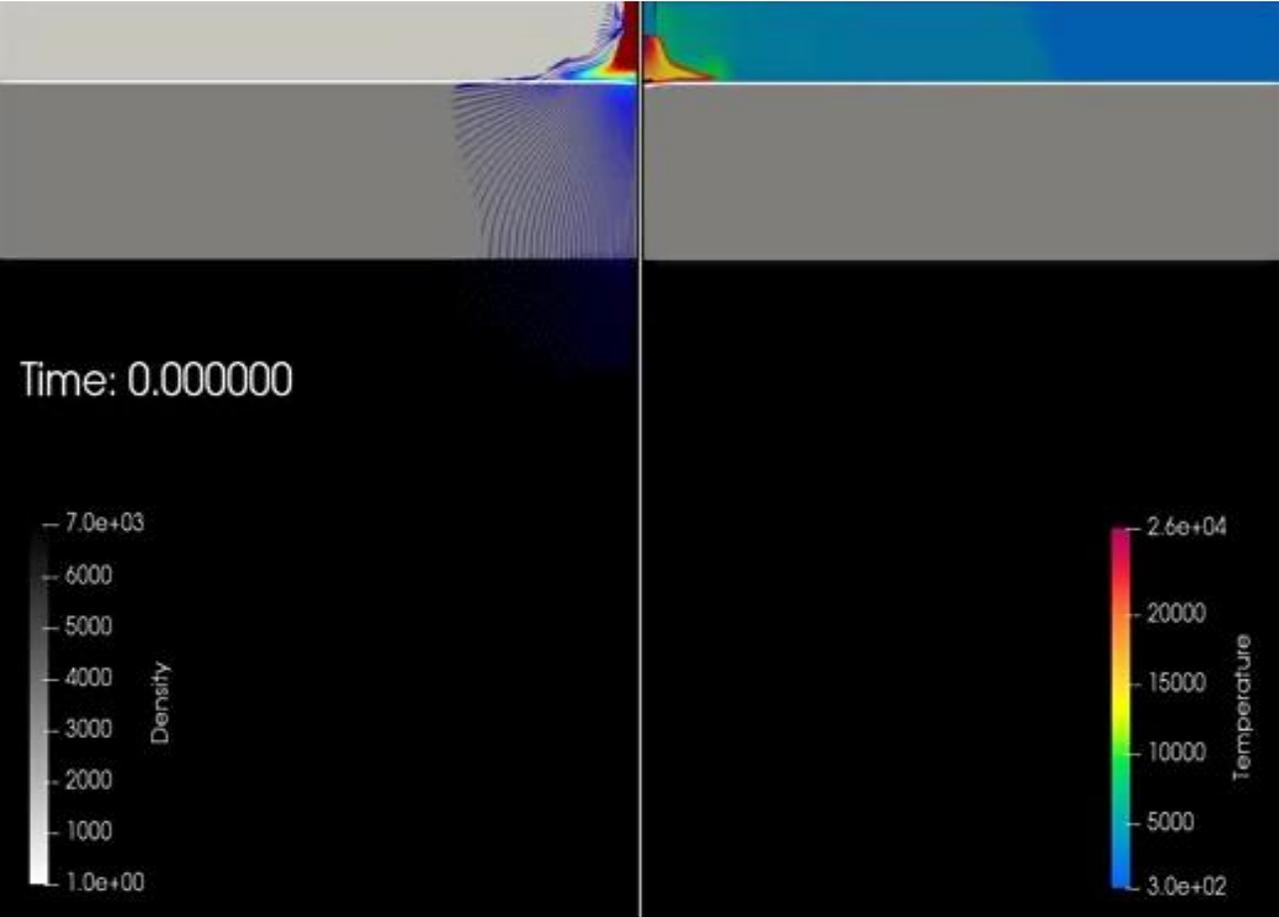
Arc Path

Temperature

20 kAmp Arc Impingement

I = 20 K amps

Arc Gap = 0.05 m



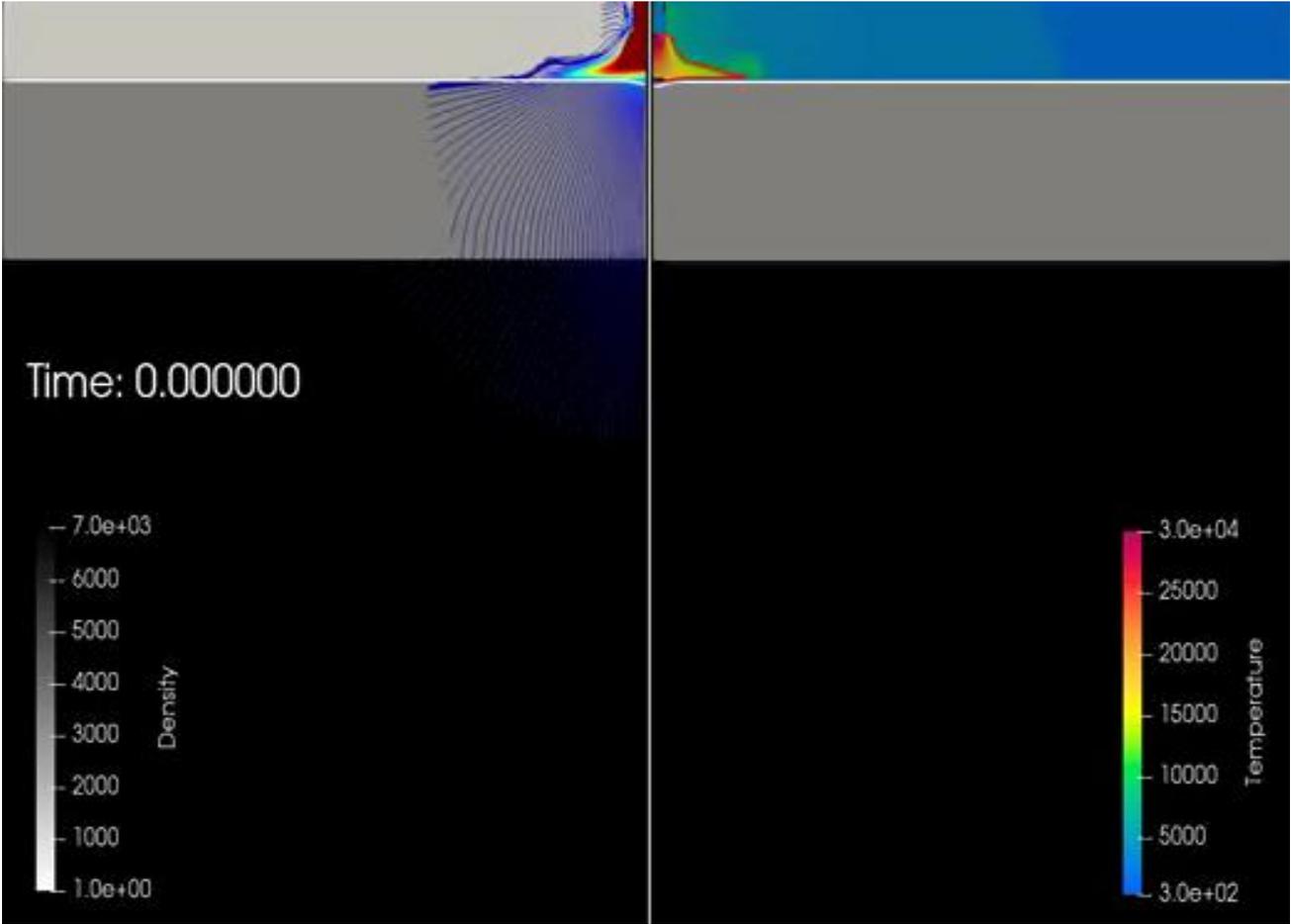
Arc Path

Temperature

30 kAmp Arc Impingement

I = 30 K amps

Arc Gap = 0.05 m



Arc Path

Temperature

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Closing remark

Arc simulation

- Aerodynamic instabilities increases voltage drop significantly
- Accounting for compressibility damps the flow from 10 000 m/sec to 3 500 m/sec
- Compressibility upturns voltage drop along the arc from average of 320 volt to 430 volt

Arc impingement:

- Slag layer protects the liquid metal from getting direct exposure to high arc temperatures and being exposed to air directly
- 20 kA increases the mixing of slag and metal significantly
- Arc impingement depth exceeds 0.7 m for 20 kA and 30 kA

Appendix

Mathematical model

- In order to solve the flow, thermal and electromagnetic field these equations are solved :

- Flow equations:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \mathbf{u} = 0$$

$$\frac{d \rho \mathbf{u}}{dt} = -\nabla p + \nabla \cdot (\mu \nabla \mathbf{u}) + \frac{1}{\mu_0} (\mathbf{J} \times \mathbf{B}) + \rho \mathbf{g}$$

- Energy equation:

$$\frac{\partial}{\partial t} (\rho c_p T) + \nabla \cdot (\rho c_p \mathbf{u} T) = \nabla \cdot (k \nabla T) + J_{heat} + Q_{rad loss} \quad (J_{Heat} = \frac{J^2}{\sigma})$$

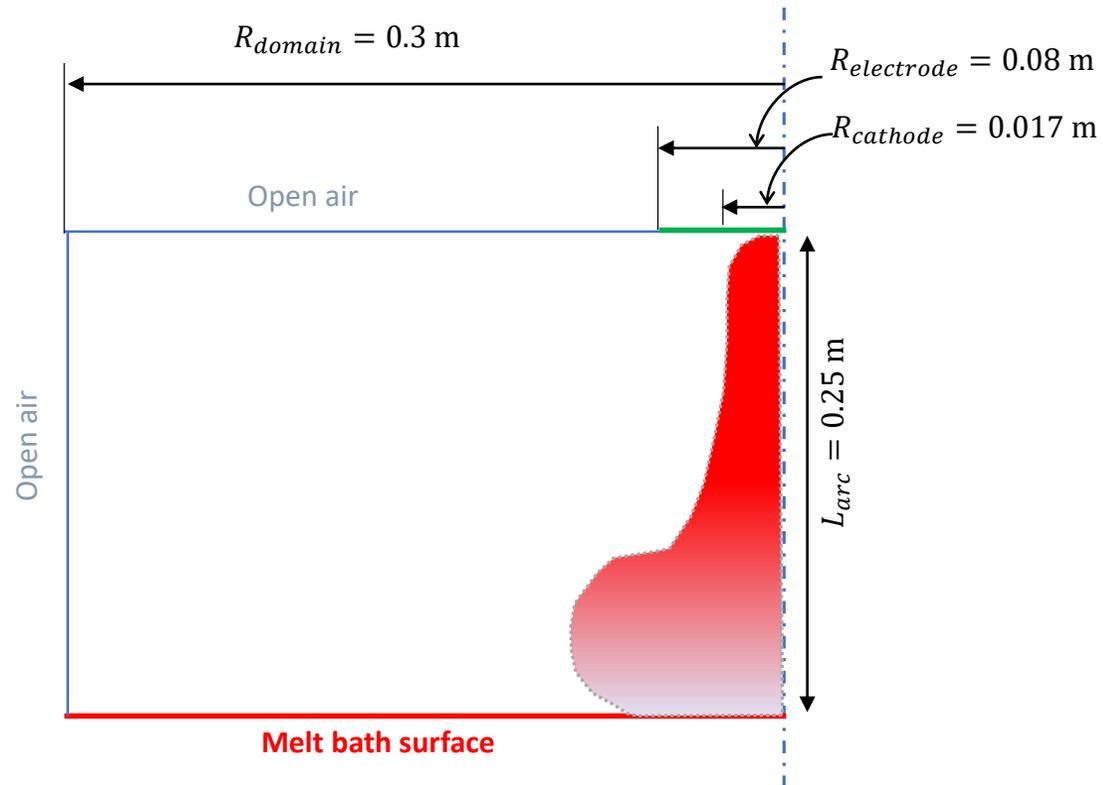
- Induction Equation:

$$\frac{\partial \mathbf{B}_\theta}{\partial t} + \nabla \cdot (\mathbf{u} \mathbf{B}_\theta) = \nabla \cdot \left(\frac{1}{\sigma \mu_0} \nabla \mathbf{B}_\theta \right) + \frac{\partial}{\partial r} \left(\frac{1}{r \sigma \mu_0} \right) \mathbf{B}_\theta - (\partial_z (u_\theta b_z) + \partial_r (u_\theta b_r))$$

- ρ density
- μ_0 magnetic permeability
- \mathbf{g} gravitational acceleration
- c_p specific heat
- k thermal conductivity
- J_{heat} joule heating
- $Q_{rad loss}$ radiation loss
- σ electrical conductivity

Boundary conditions single phase electric arc

- The geometry is modeled in 2D axisymmetric domain
- The arc gap is taken to be 25 cm
- And the electrode radius is set to 8 mm
- We assume that we have a constant current density at the cathode spot which gives 1.7 cm for 40 kAmp



Boundary conditions single phase electric arc

Boundary conditions

$$I_0 = 40 \text{ kA}$$

$$B_\theta = \frac{I_0 \mu_0 r}{2\pi R_c^2}$$

$T = 4000 \text{ K}$
No-slip wall

$$B_\theta = \frac{I_0 \mu_0}{2\pi r}$$

$$\frac{\partial h}{\partial z} = 0$$

$$P = 1 \text{ atm}$$

$$B_\theta = \frac{I_0 \mu_0}{2\pi r}$$

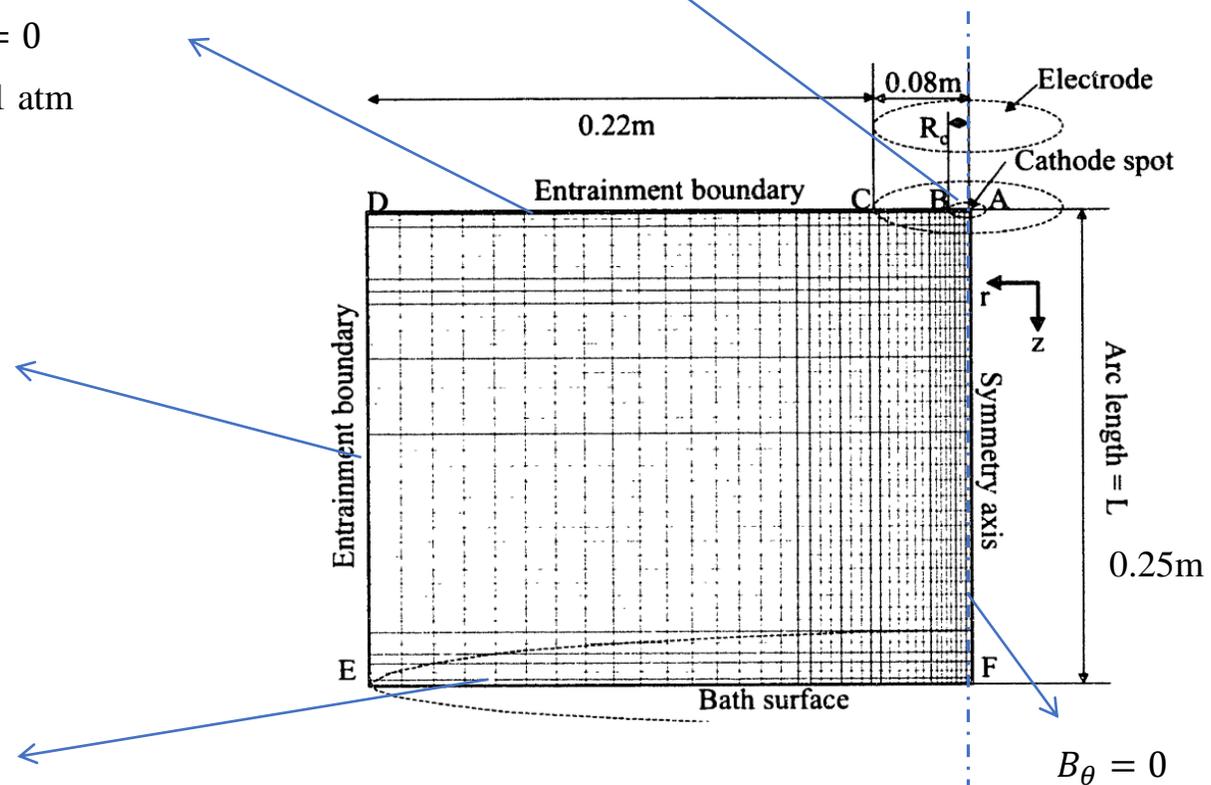
$$\frac{\partial h}{\partial r} = 0$$

$$P = 1 \text{ atm}$$

$$\frac{\partial B_\theta}{\partial z} = 0$$

$$T = 1800 \text{ K}$$

$$\text{No-slip wall}$$

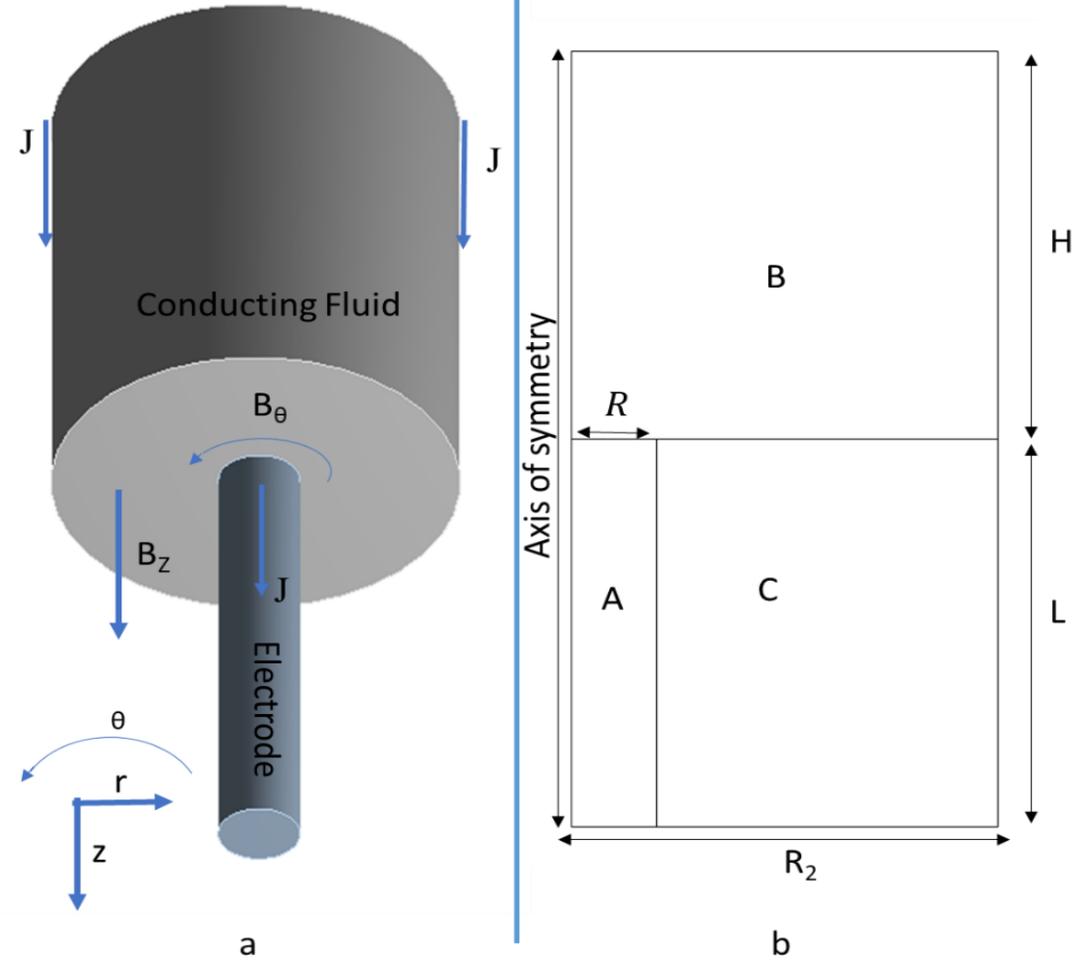


$$B_\theta = 0$$

Liquid metal simulation

Geometry of the 2D axisymmetric space:

- A is the electrode,
- B is the conducting fluid zone,
- C is a non-conducting enclosure

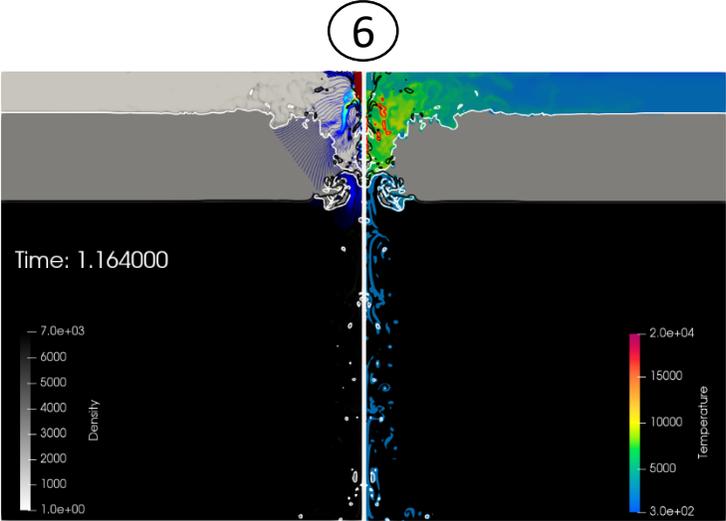
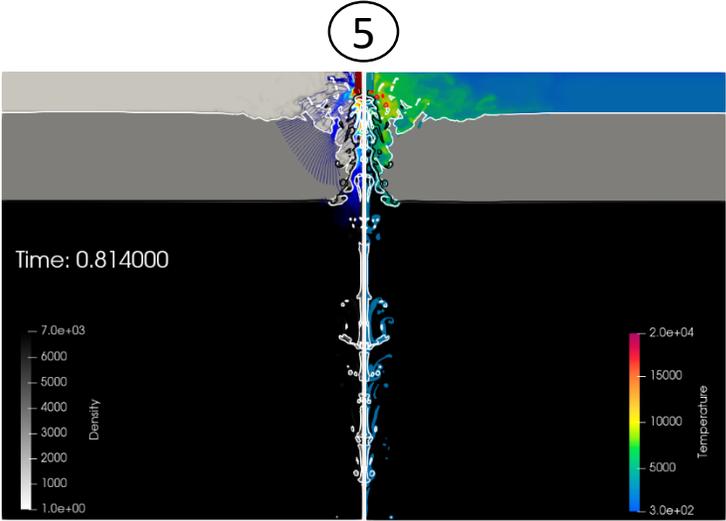
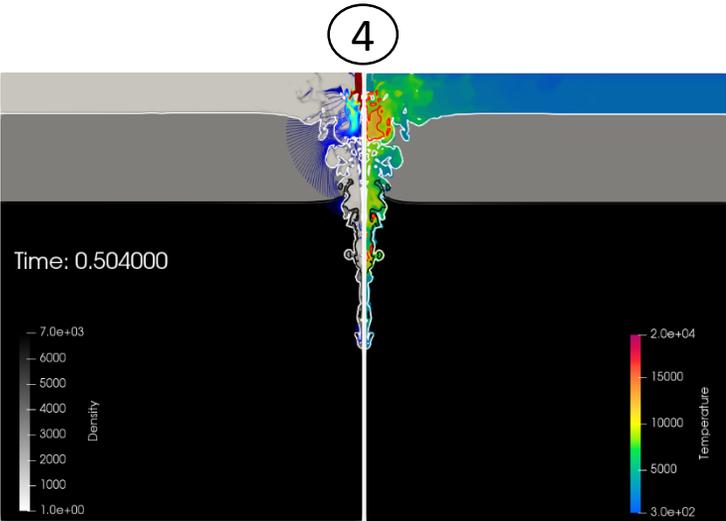
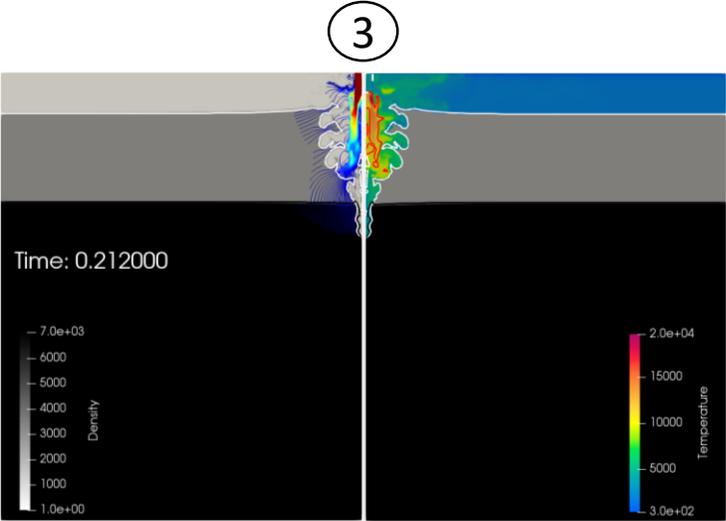
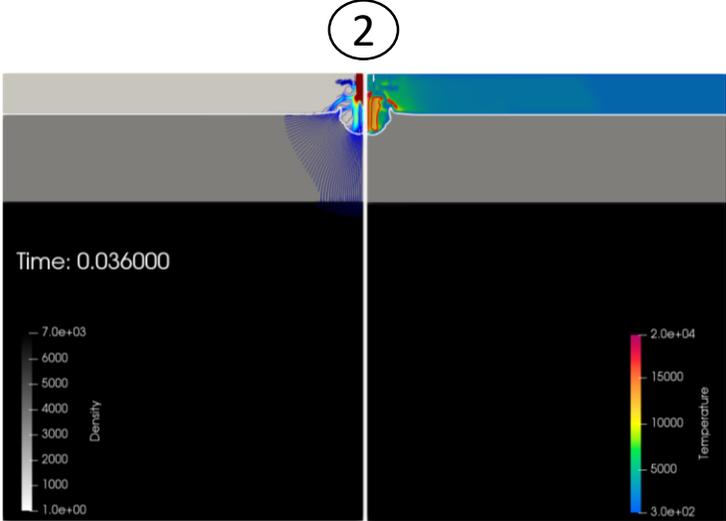
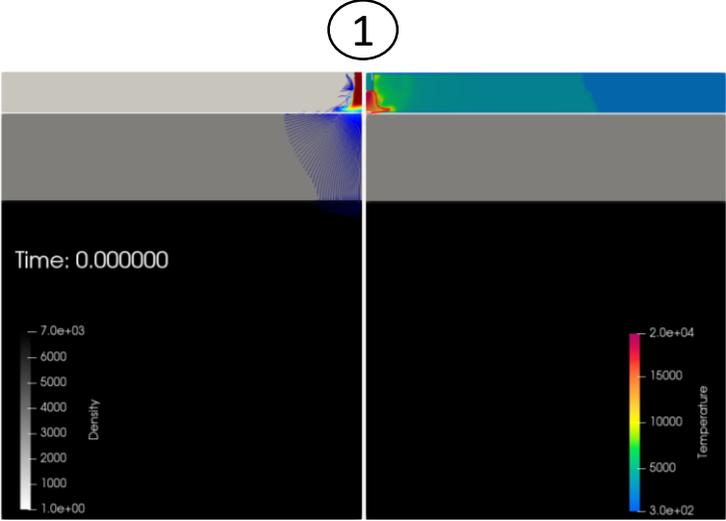


Boundary conditions

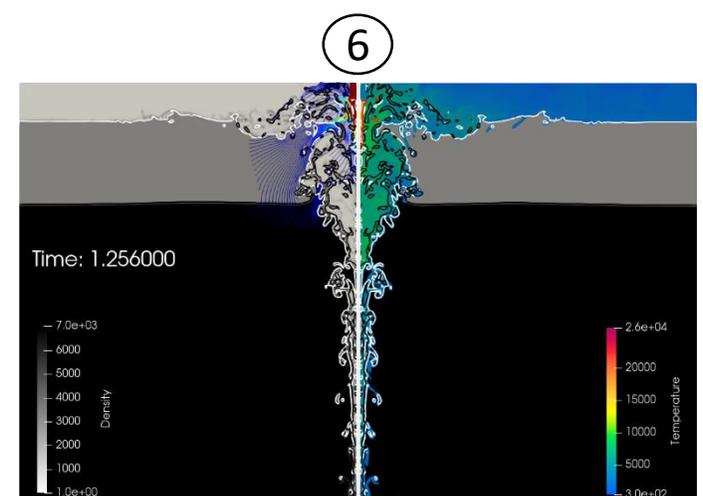
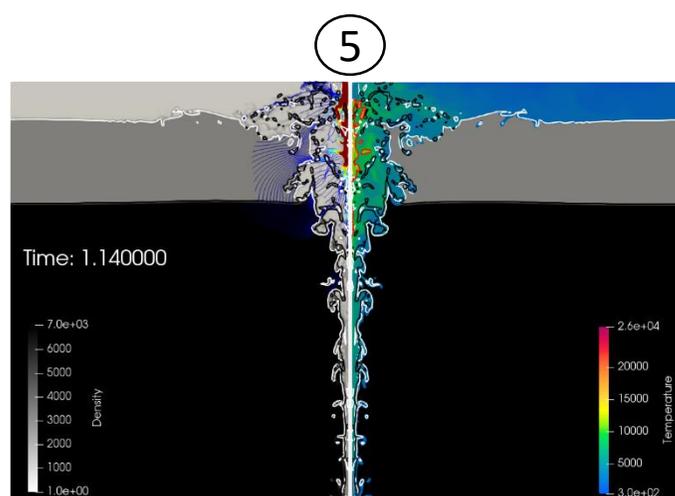
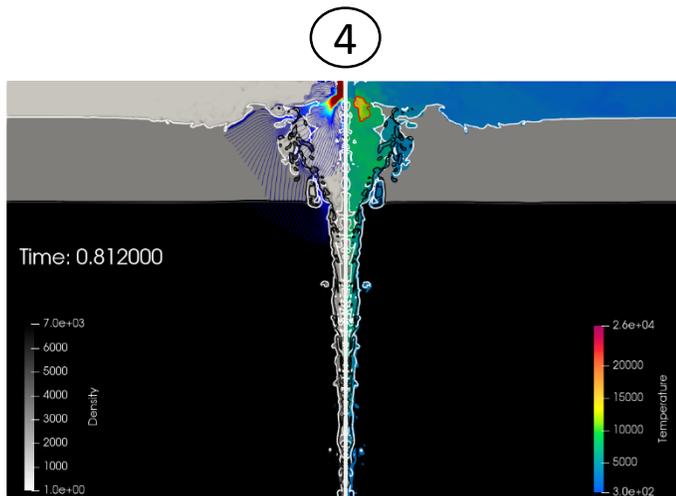
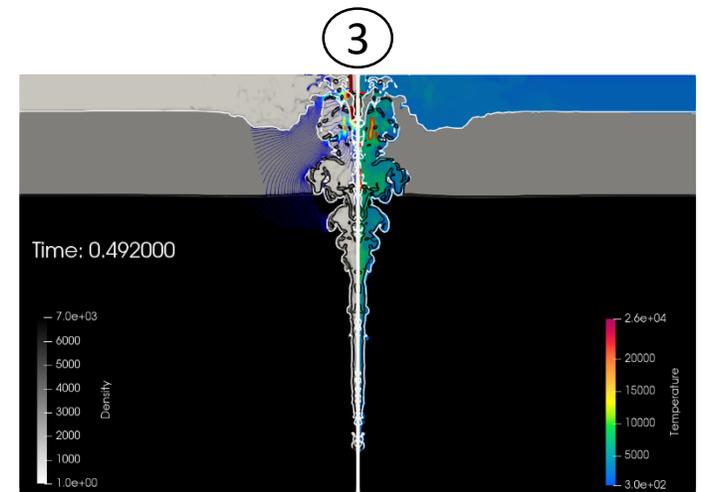
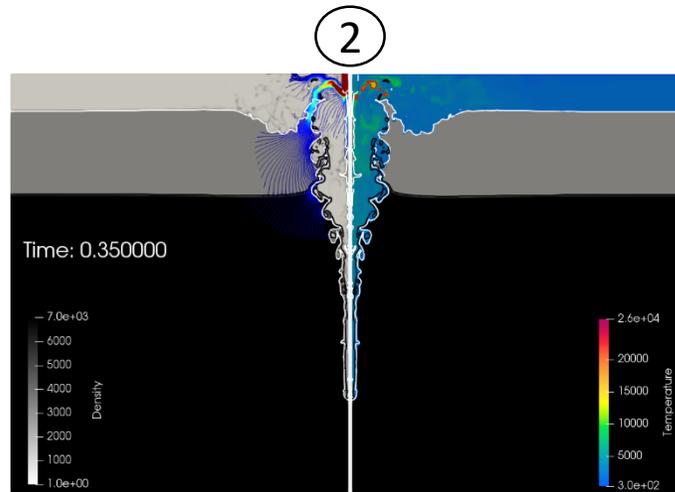
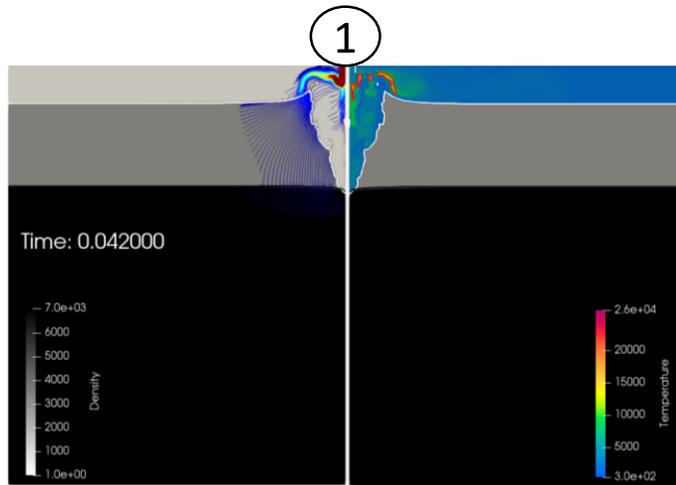
- 10 ,20, 30 KA
- Electrode R =8,12 ,15 mm
- Arc Gap = 0.05 m
- Metal depth = 0.73 m
- Slag depth = 0.2 m
- No external magnetic field
- Sides and bottom are adiabatic
- Top is cooled and have a temperature of 500 K



Arc Impingement

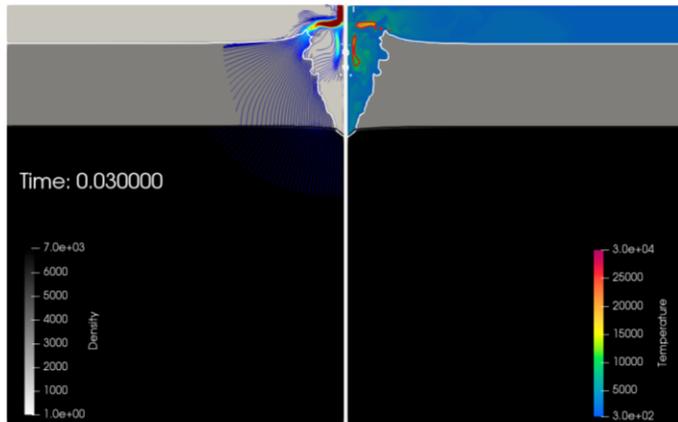


Arc Impingement

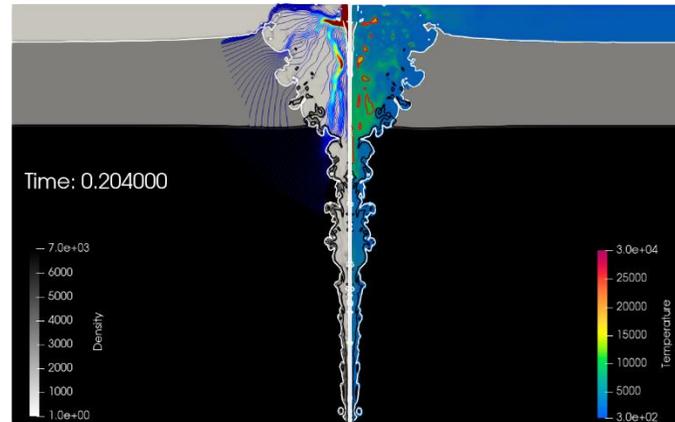


Arc Impingement

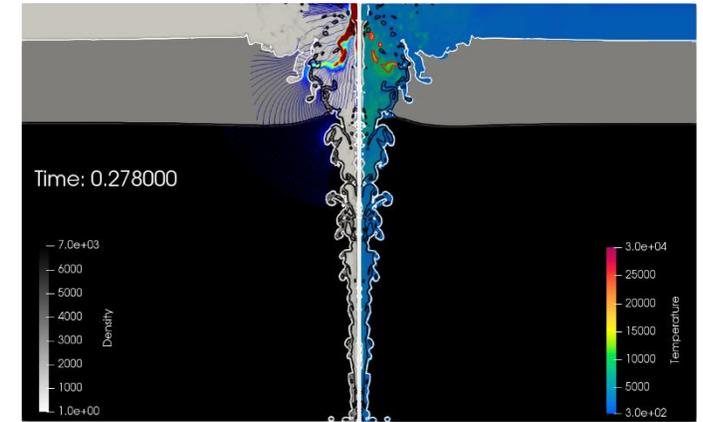
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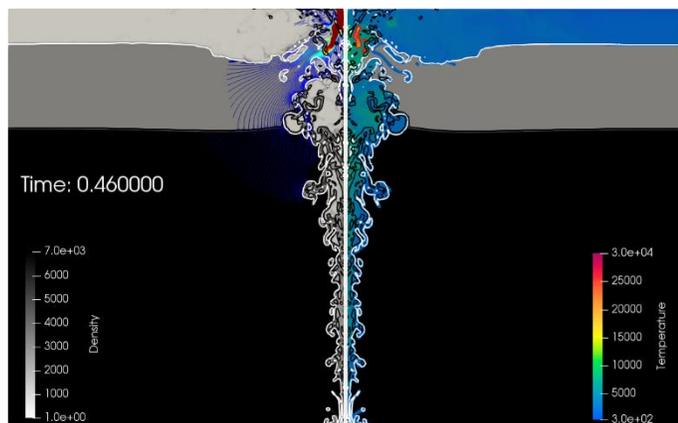
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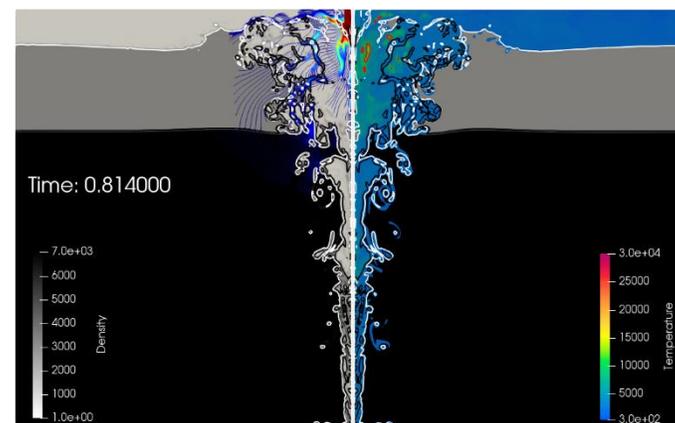
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