

Static dissolution evaluation of dolomite-based materials in EAF-type slag

S. Scheibera^{a)}, E. Cheremisina^{a)}, J. Rieger^{a)}, J. Schenk^{b)},
F. Firsbach^{c)}, W. Johnson^{c,d)}, T. Chopin^{c)}, M. Nispel^{c)}

a) K1-MET GmbH

b) Montanuniversität Leoben, Chair of Ferrous Metallurgy

c) Lhoist Business Innovation Center (BIC)

d) Lhoist North America (LNA)

stefanie.scheiber@k1-met.com

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K1-MET at a glance

Motivation - Development of resource intensive processes



K1-MET – Competence Center for Excellent Technologies in Advanced Metallurgical and Environmental Process Development
→ Austrian funded research program

Current funding phase 2019–2023
Budget of this phase: 22.7 M€

Financing: 45 % public funding

- 30 % Governmental funding
- 15 % Federal states Upper Austria, Styria, Tyrol
- 5 % Scientific partners
- 50 % Industrial partners

Currently 75 employees

- Thereof 65 researchers (master and PhD students, post-docs, Senior Experts)

Locations

- Linz
- Leoben



Four symbiotic areas:

- **Area 1: Raw Materials and Recycling**
Endeavours the best possible utilisation of all resources and searches for residue treatment and recycling solutions
- **Area 2: Metallurgical Processes**
Unites the core topics of metallurgical process developments
- **Area 3: Low Carbon Energy Systems**
Is dedicated to the developments of carbon-lean steel production
- **Area 4: Simulation and Analyses**
Represents the enveloping area for numerical developments and data analyses

(1) K1-MET at a glance

(2) Introduction

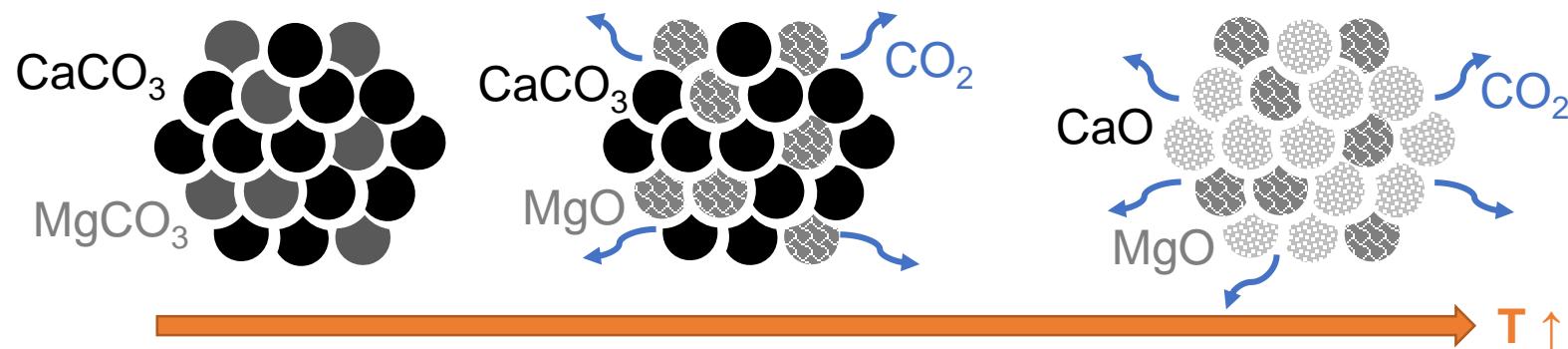
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- Basic additives to adapt slag chemistry and enable refining
- Advantages of dolomite-based materials due to MgO saturation
- Stepwise calcination of $\text{CaMg}(\text{CO}_3)_2$ to MgO ($600\text{--}700\text{ }^\circ\text{C}$) and CaO ($700\text{--}900\text{ }^\circ\text{C}$)



- Cracks and pores resulting from decomposition
- Heat losses because of transport to steelmaking industry

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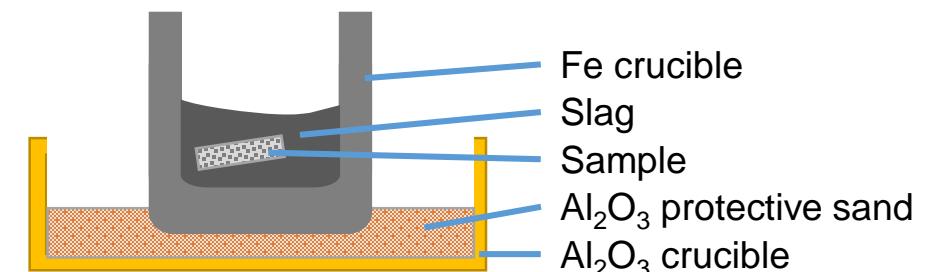
Experimental setting

High-temperature static dissolution investigation

- Heating of Gero vertical high-temperature furnace to 1,450 °C under N₂ atmosphere
- Mixing of chemically pure oxides according to target composition
- Melting of EAF slag at target temperature in the pure iron crucible
- Insertion of dolomite-based samples of varying composition and calcination condition
- Isothermal reaction duration fixed to 10 min
- Disc sample not extracted at the end of dissolution test
- Quenching of crucible, slag and immersed sample in liquid nitrogen

EAF slag	MgO	Al ₂ O ₃	SiO ₂	CaO	MnO	FeO
Oxide [wt.-%]	–	10	25	25	8	32

	Raw 1	Raw 2
	Soft-burned 1	Soft-burned 2
	Hard-burned 1	Hard-burned 2



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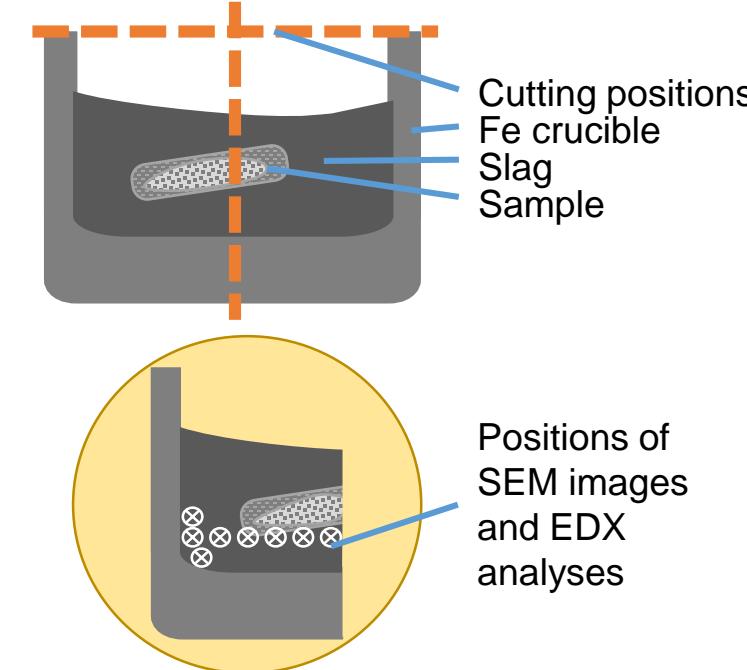
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Methodology of slag chemistry determination

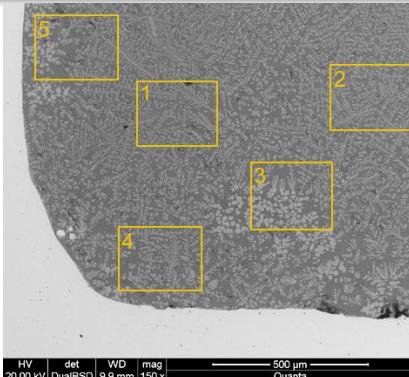
From EDX analysis to oxide profiles and bulk slag chemistry

- Water-free cutting and metallographic preparation of embedded slags
- SEM/EDX analysis using FEI QUANTA 200 in low vacuum mode
- Pure iron crucible as reference position
- Multiple small area analyses (270 µm by 200 µm) of bulk slag on images in periodical distances of 2 mm
- Exclusion of interfacial layers and remaining undissolved sample pieces
- Calculation of mean oxide composition per image and plot of concentration profile
- Brittle behaviour of slag and thermal stresses cause material losses during cutting and grinding → cracking and crumbling of slag
- Total mean value of all chemistries in the plot for examination of dissolution behaviour dependent on calcination condition

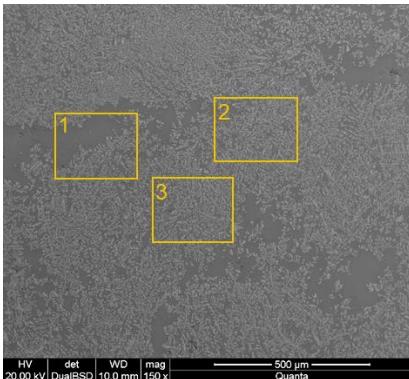


Extract from SEM/EDX analyses of raw dolomite 1

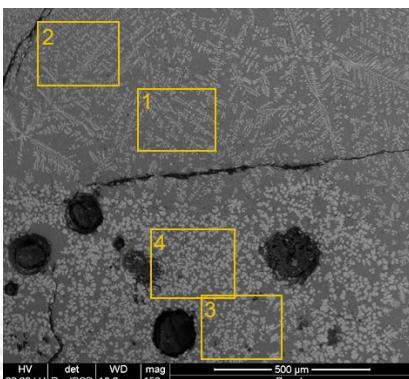
Selection of bulk slag areas without morphology changes



Oxide [wt.-%]	MgO	Al ₂ O ₃	SiO ₂	CaO	MnO	FeO
1	4.3	8.3	23.6	26.9	5.3	31.5
2	4.2	8.5	23.7	26.1	5.7	31.7
3	5.8	7.9	20.5	21.9	6.0	37.8
4	4.5	8.3	22.5	24.5	5.2	34.9
5	4.8	8.0	22.3	25.0	5.2	34.8



Oxide [wt.-%]	MgO	Al ₂ O ₃	SiO ₂	CaO	MnO	FeO
1	3.7	9.2	26.3	27.8	5.3	27.7
2	4.2	8.2	23.0	24.3	6.1	34.2
3	4.0	8.2	23.9	25.0	6.0	32.9



Oxide [wt.-%]	MgO	Al ₂ O ₃	SiO ₂	CaO	MnO	FeO
1	5.1	8.4	24.3	26.2	5.9	30.1
2	4.7	8.5	24.1	27.0	5.2	30.4
3	9.3	7.7	21.3	22.3	6.1	33.3
4	10.5	6.6	19.1	19.0	6.5	38.3

Pic.	Distance to wall [mm]	MgO	Al ₂ O ₃	SiO ₂	CaO	MnO	FeO
		[wt.-%]	[wt.-%]	[wt.-%]	[wt.-%]	[wt.-%]	[wt.-%]
1	0.7	4.5	8.3	23.0	25.6	5.4	33.2
2	0.5	4.2	8.7	23.3	26.4	5.8	31.5
3	2.6	4.3	8.6	23.8	27.5	5.6	30.2
4	4.4	4.0	8.7	24.1	25.7	6.0	31.5
5	6.5	3.8	9.1	25.4	27.4	5.7	28.6
6	8.6	3.9	8.6	24.4	25.7	5.8	31.6
7	10.6	4.2	8.3	23.7	25.2	5.9	32.8
8	12.5	4.2	8.5	23.6	25.8	6.0	32.1
9	14.6	4.3	8.5	23.5	26.0	5.9	31.7
10	16.7	4.4	8.5	24.1	27.0	5.6	30.4
11	18.6	4.5	8.4	23.6	27.3	5.7	30.5
12	20.6	4.3	8.6	24.4	28.4	5.6	28.7
13	22.5	4.4	8.5	23.6	27.1	5.8	30.6
14	14.5	4.1	9.3	25.2	27.0	5.4	29.0
15	14.3	4.9	8.6	23.0	24.2	5.3	34.0
16	14.6	4.8	8.6	23.6	27.8	5.5	29.7
17	14.2	4.8	8.2	24.0	27.4	5.5	30.2
18	6.2	4.9	8.6	24.7	26.4	5.7	29.7
20	5.0	5.2	8.4	24.0	25.9	5.8	30.8
22	6.5	4.9	8.5	24.2	26.6	5.5	30.3
Total mean value		4.4	8.6	24.0	26.5	5.7	30.8
Standard deviation		0.4	0.2	0.6	1.0	0.2	1.5

Original slag: 0MgO-10Al₂O₃-25SiO₂-25CaO-8MnO-32FeO

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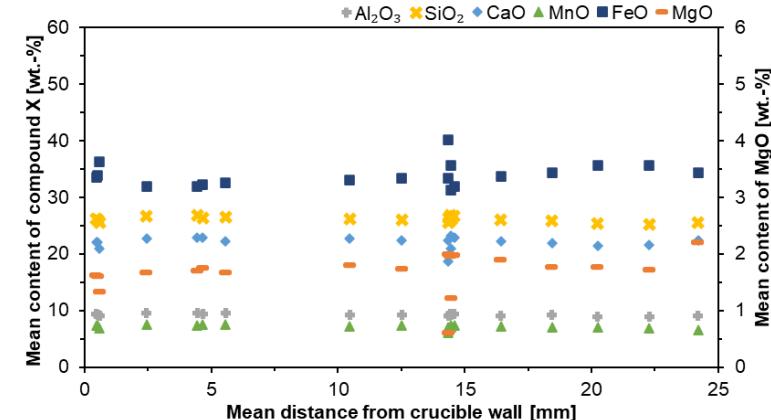
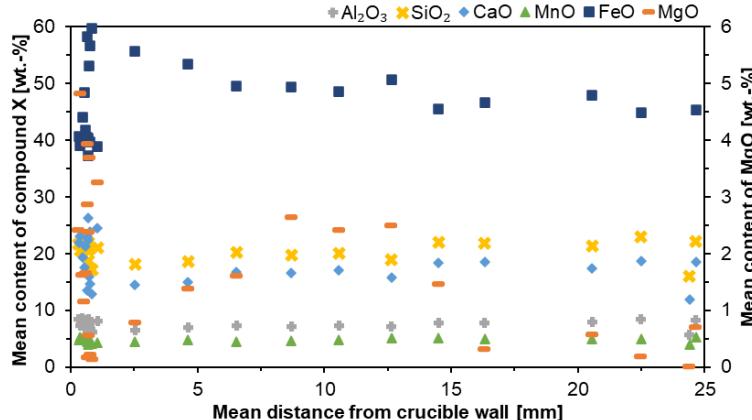
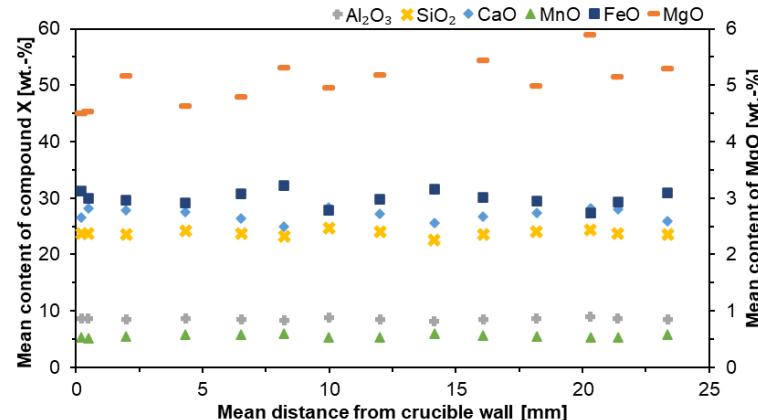
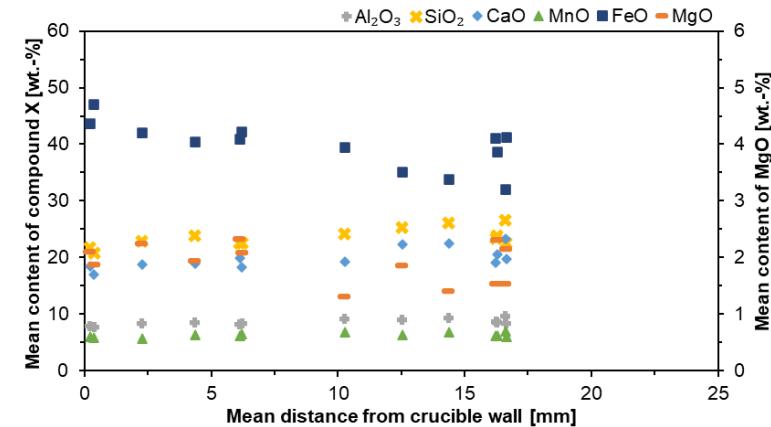
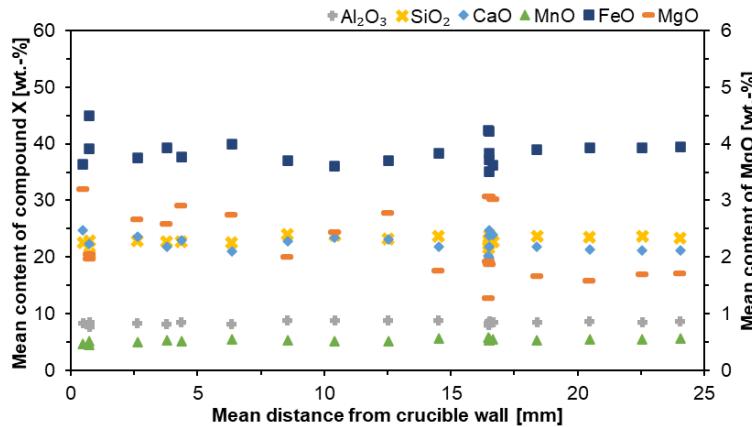
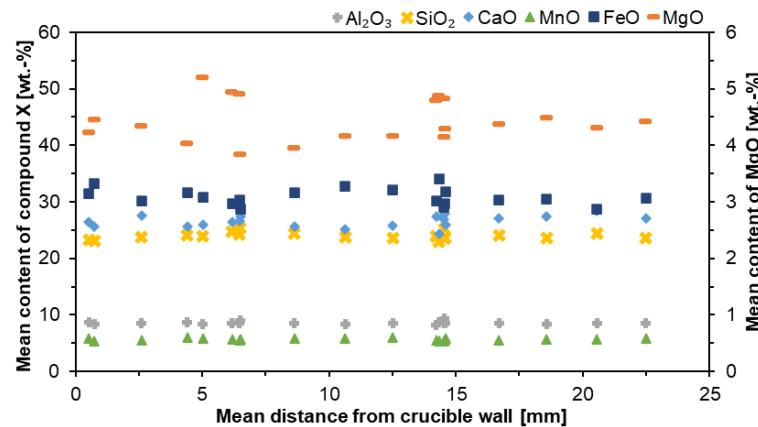
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Bulk slag oxide concentrations

Distribution profiles as well as average amounts of MgO and CaO

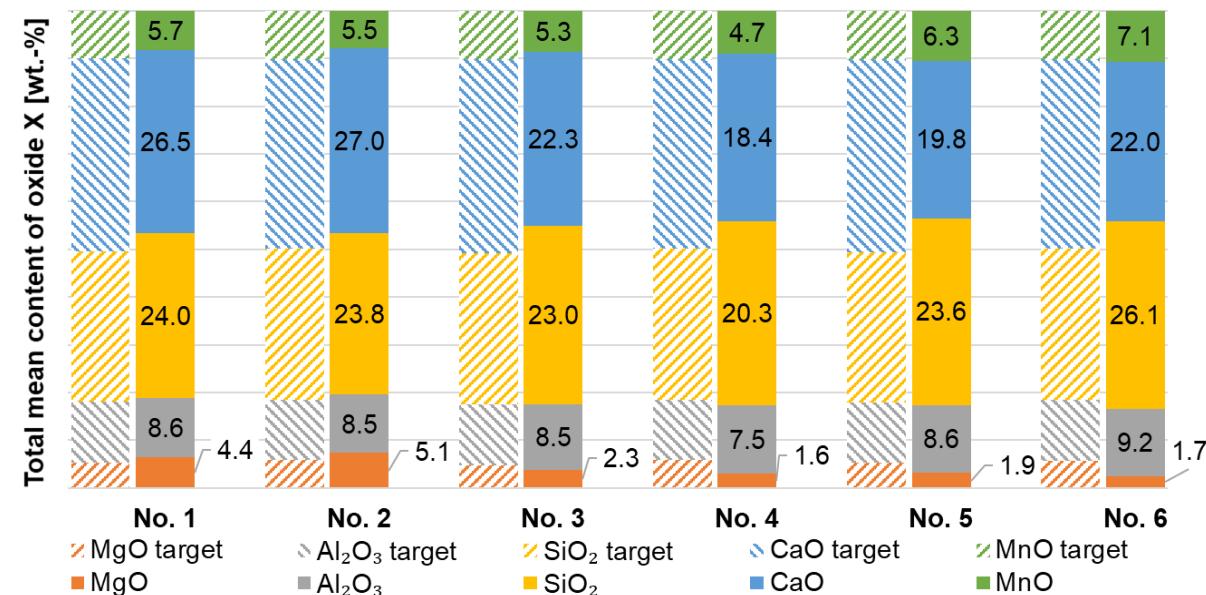


Comparison of dolomite dissolution

Influences of calcination conditions raw, soft- and hard-burned

- Excluding the FeO for comparison of dissolution behaviour
- Raw dolomite samples exceeded the MgO target and more than 95 % of CaO dissolved
- Decrease to relative levels of 78 % MgO and 89 % CaO for soft-burned dolomite 1
- Very high FeO content in test no. 4 suppressed other oxides in analyses (cf. Al_2O_3 and MnO; 52 % MgO and 88 % CaO dissolved)
- MgO level of hard-burned dolomite 1 higher than of hard-burned dolomite 2 (60 % vs. 44 %), opposite effect for CaO (81 % vs. 84 %)

No.	Dolomite condition	Target content of oxide X [wt.-%]					
		MgO	Al_2O_3	SiO_2	CaO	MnO	FeO
1	Raw 1	3.8	9.0	22.5	28.8	7.2	28.7
2	Raw 2	4.2	9.0	22.5	28.3	7.2	28.8
3	Soft-burned 1	3.4	9.0	22.6	28.9	7.2	28.8
4	Soft-burned 2	4.2	9.0	22.5	28.3	7.2	28.8
5	Hard-burned 1	3.7	9.0	22.5	28.9	7.2	28.7
6	Hard-burned 2	4.1	9.0	22.6	28.2	7.2	28.9



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- The raw dolomite materials dissolved quickly, as the resulting MgO concentrations were high (no MgO in starting slag composition).
- Additionally, the CaO contents were above the SiO₂ amounts, indicating additional CaO uptake from specimens.
- It was assumed that in-situ decomposing carbonates caused local stirring effects.
- The fluctuations in tests of soft- and hard-burned dolomites could indicate a slower dissolution with missing time for concentration balancing.
- The dissolution of soft-burned dolomite 1 was on a medium level, whereas the massive amount of FeO in trial with soft-burned dolomite 2 impeded a comparable evaluation of dissolution behaviour.
- The hard-burned dolomite materials showed reduced MgO and CaO dissolution, which might be caused by lower sample porosity due to sintering of particles during calcination.

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